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16th-17th December 2015, Athens Greece

Techno-Economic Evaluation on the Effects of Impurities for Conditioning and Transport of CO₂ by Pipeline

Geir Skaugen, SINTEF ER

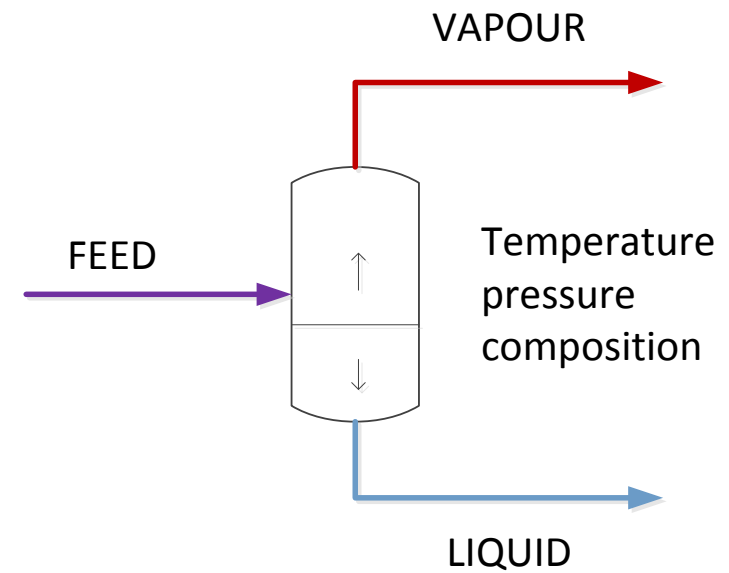
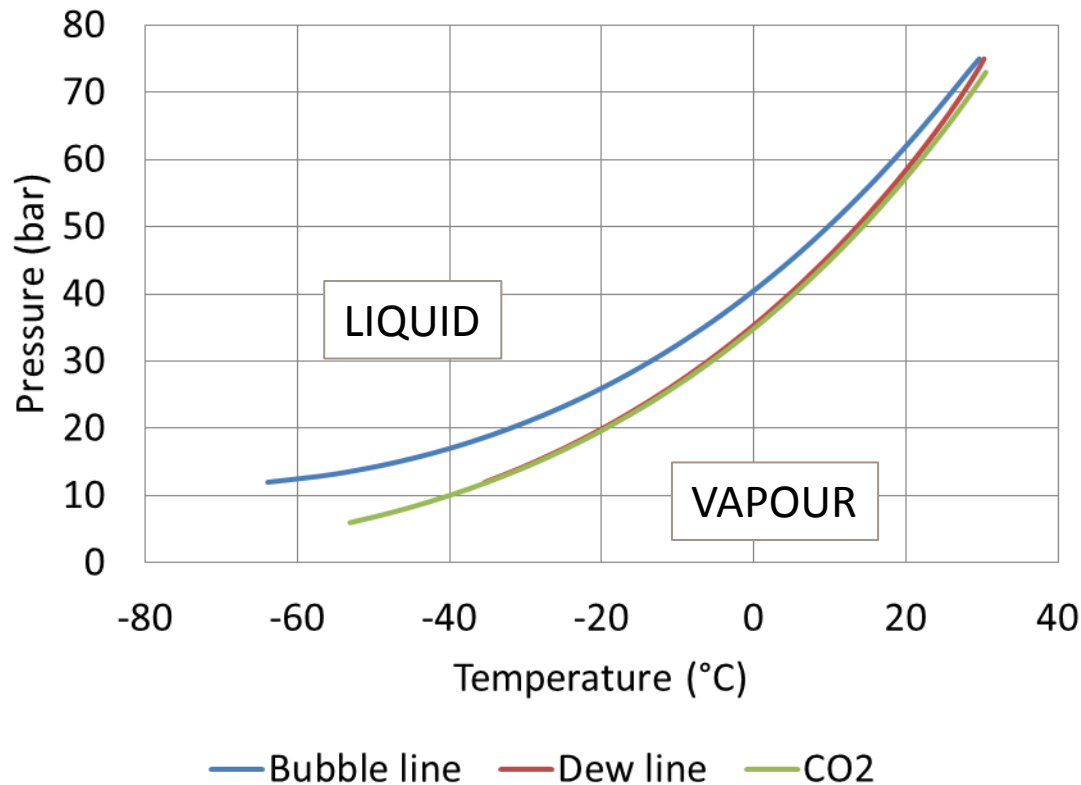
Simon Roussanaly, SINTEF ER

Introduction – Content of presentation

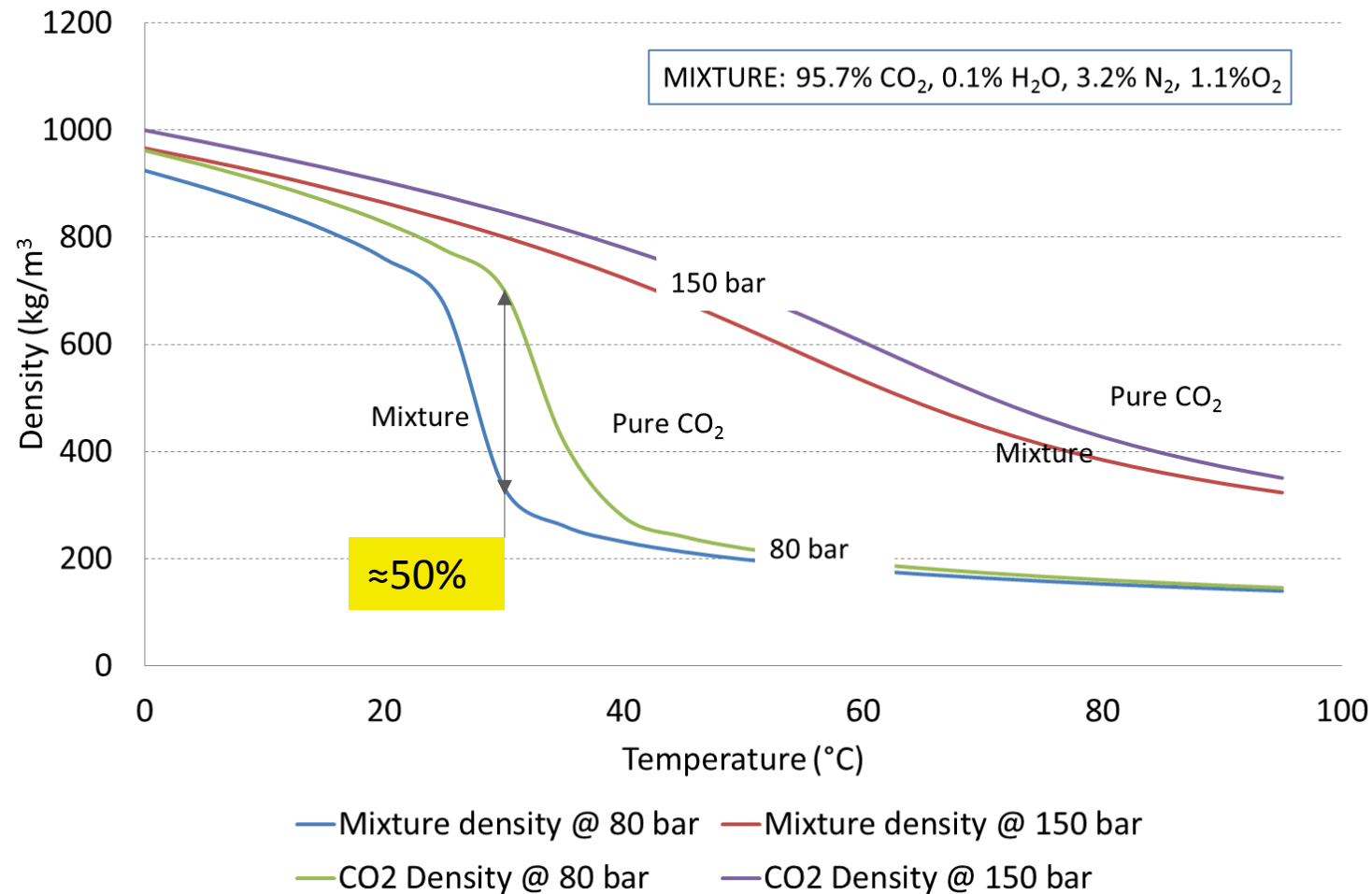
- The effect of impurities on the thermodynamic properties of CO₂ relevant for case studies
- Description case study –compressed gas for pipeline transport
- Effect of impurities on;
 - Pipeline design
 - Energy consumption
 - Cost
- Conclusion

Effects of impurities on CO₂ thermodynamic

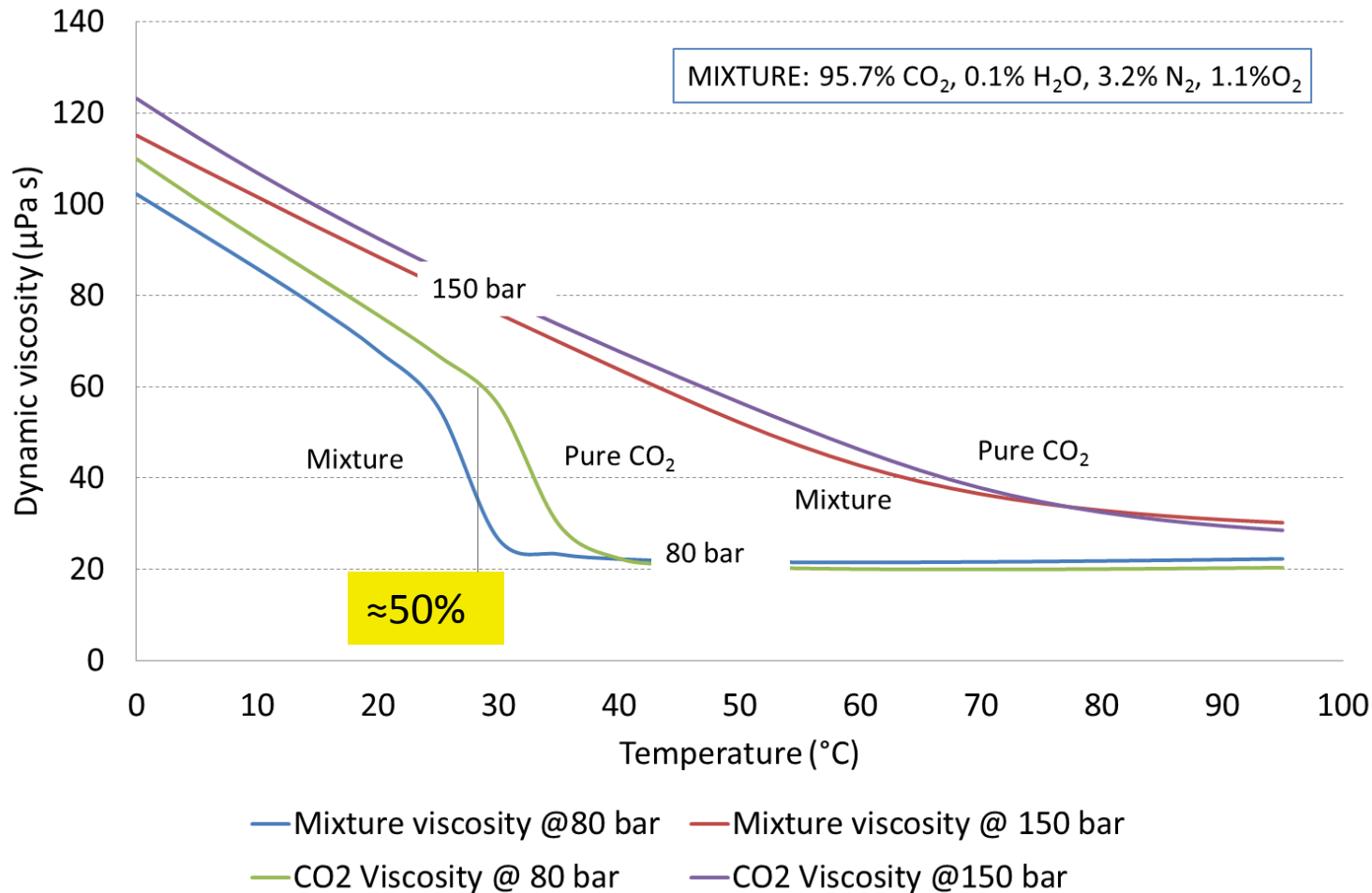
Effect of 2% N₂



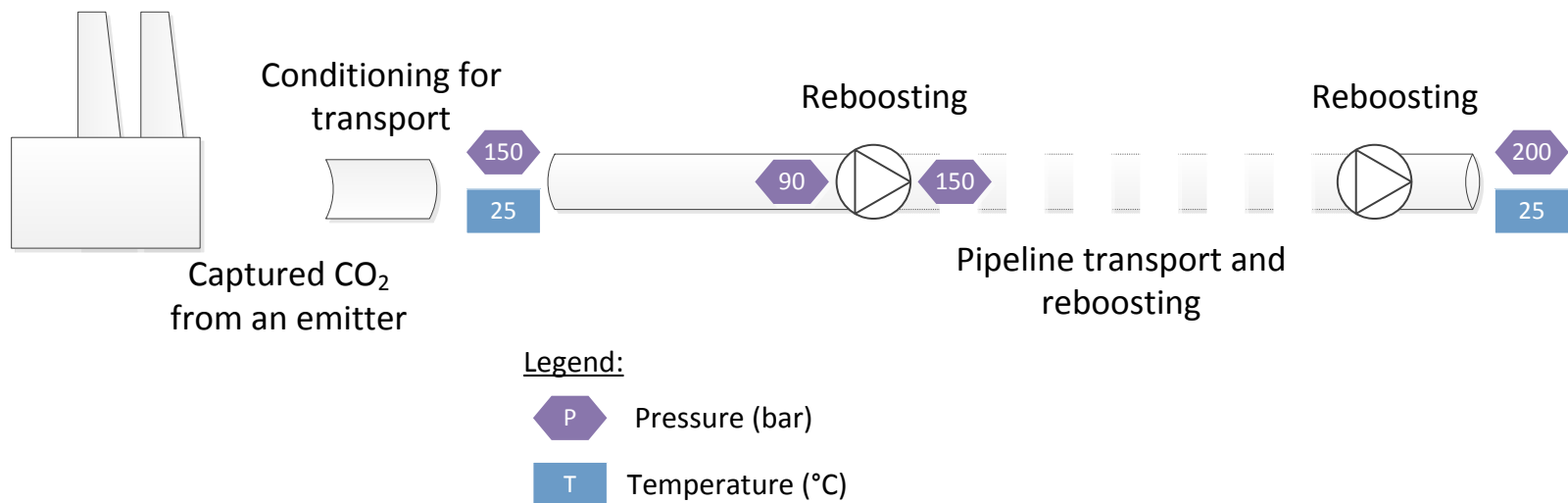
Effects of impurities on density (predictions)



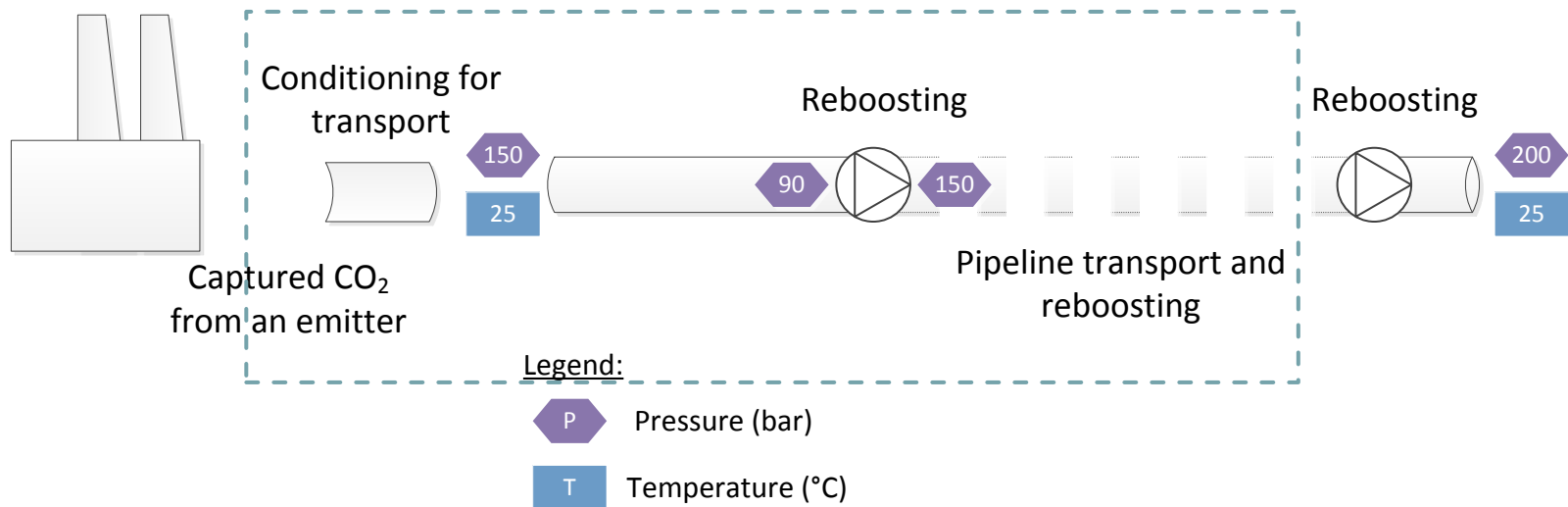
Effects of impurities on viscosity (predictions)



Pipeline transport of CO₂



Pipeline transport of CO₂



Cases, impurity levels and boundary conditions

Maximum impurity levels

CASE	CO ₂	H ₂ O	N ₂	O ₂	Methane
«BASE»	93	7			
«OXY»	88	7	3	2	
«GAS»	83	7	1		9

Initial condition: Atmospheric (1.027 bar and 25°C)

Export condition: 150 bar (35-38 °C)

Ambient temperature 15°C with low heat transfer:

- Ground thermal conductivity: 2.4 W/m K
- Ambient heat transfer: 5.0 W/m²K

Total transport distance: 500 km

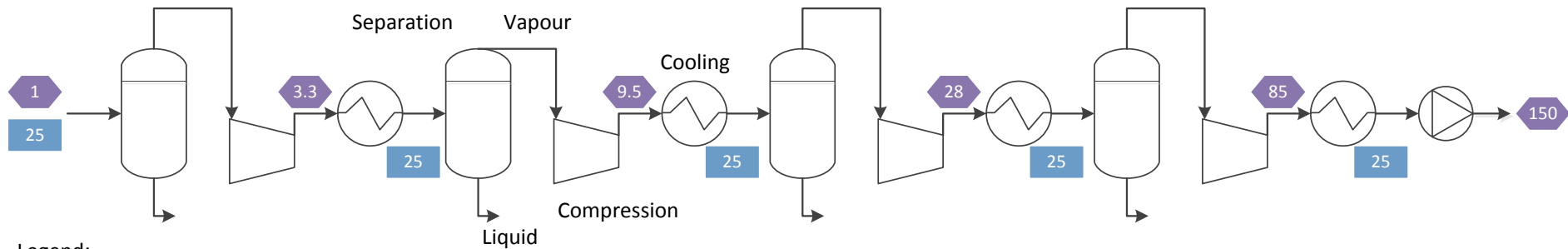
Pipeline: On-shore @ depth 1.0 m, varying diameter

Feed flow rate: 500 kg/s (13.1 MTPA)

Pipeline transport – conditioning

Feed after capture

To pipeline



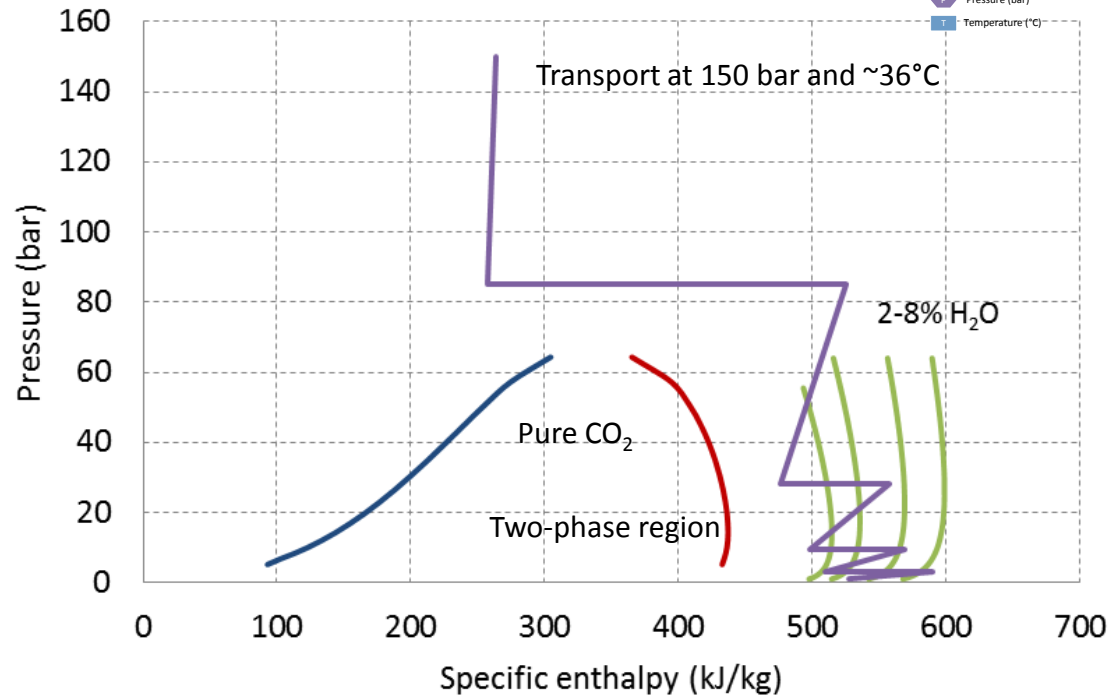
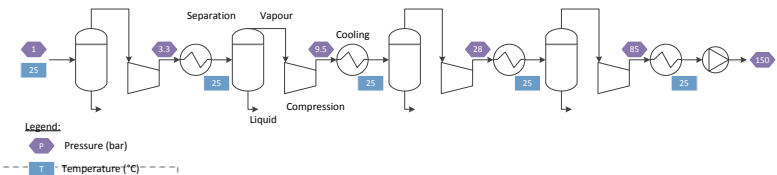
Legend:

 Pressure (bar)

T Temperature (°C)

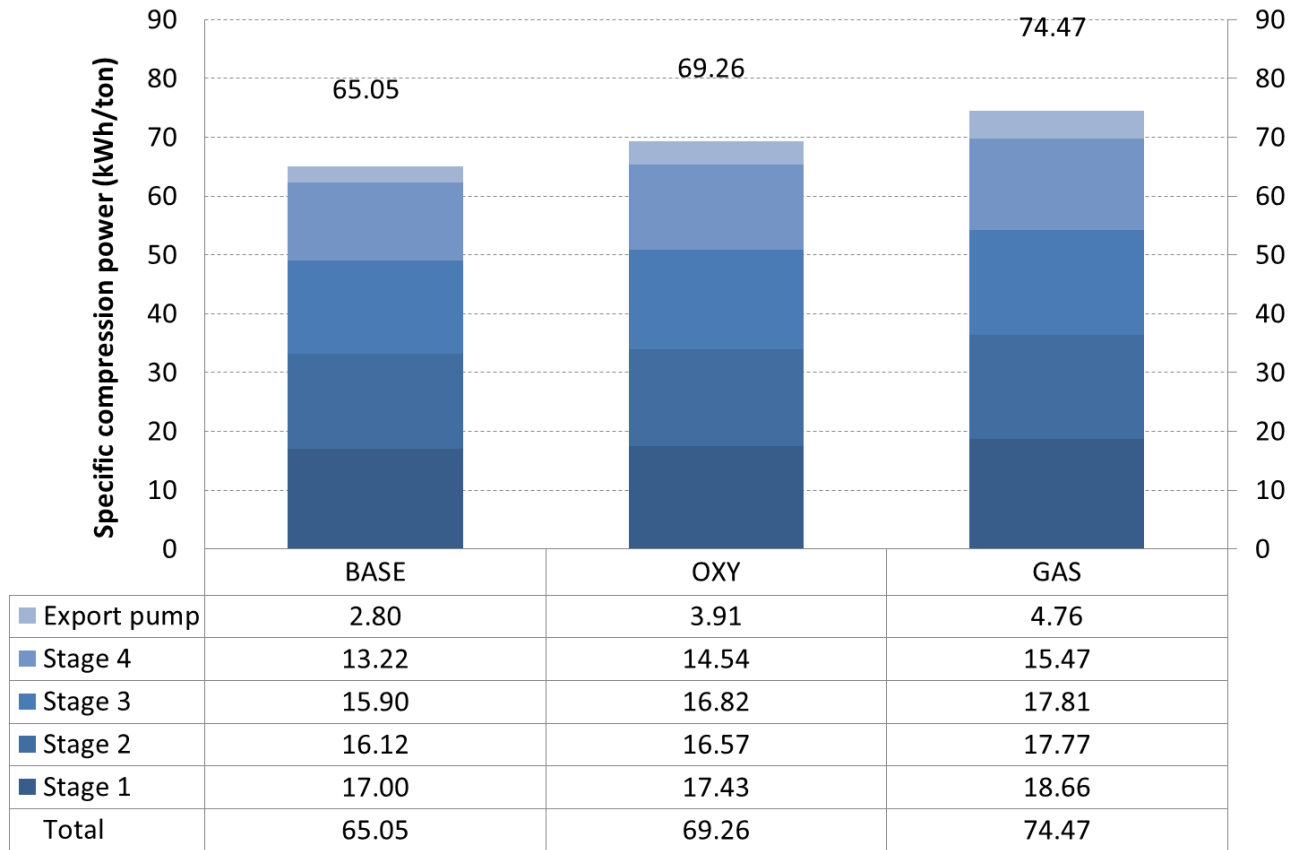
Pipeline transport – conditioning

The P-CO₂ conditioning chain

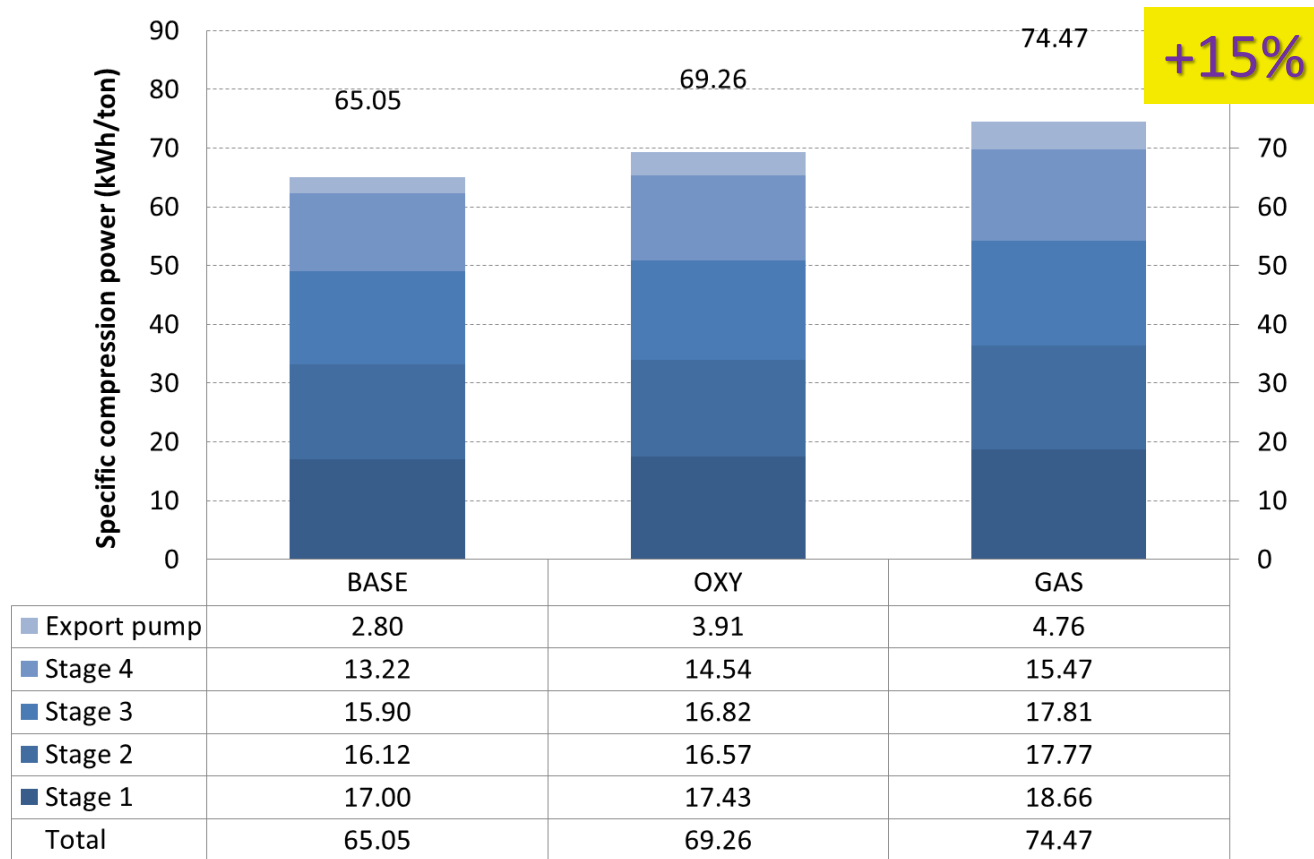


Feed – humid gas at atmospheric pressure

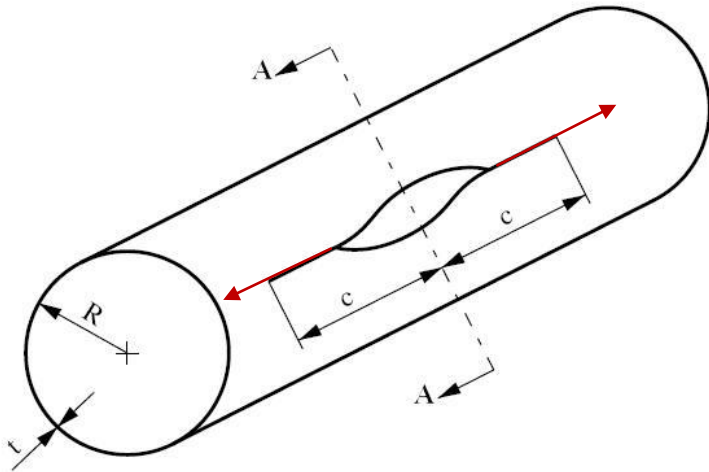
Power consumption for conditioning before export



Power consumption for conditioning for export

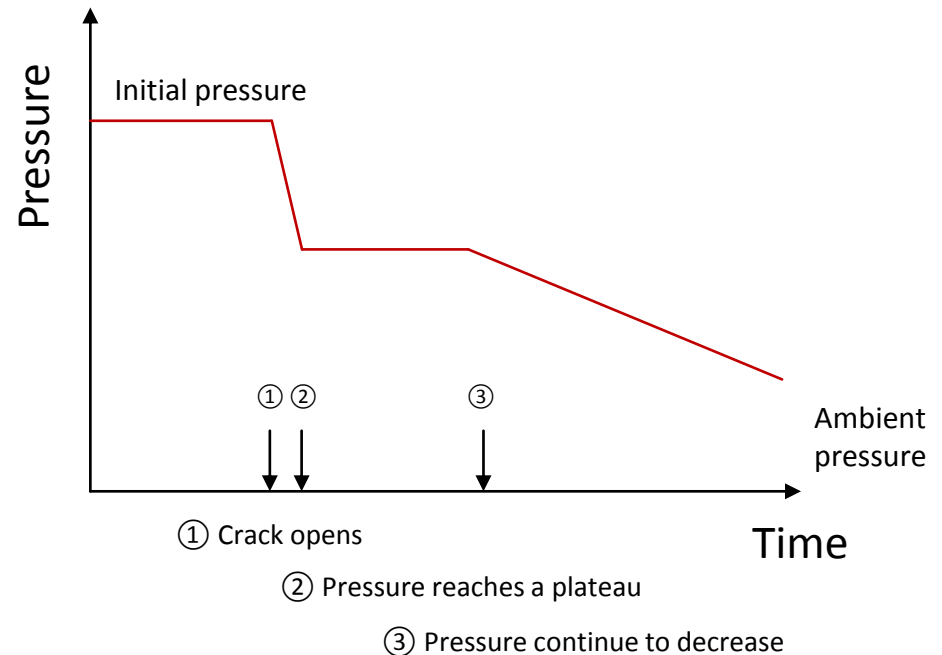
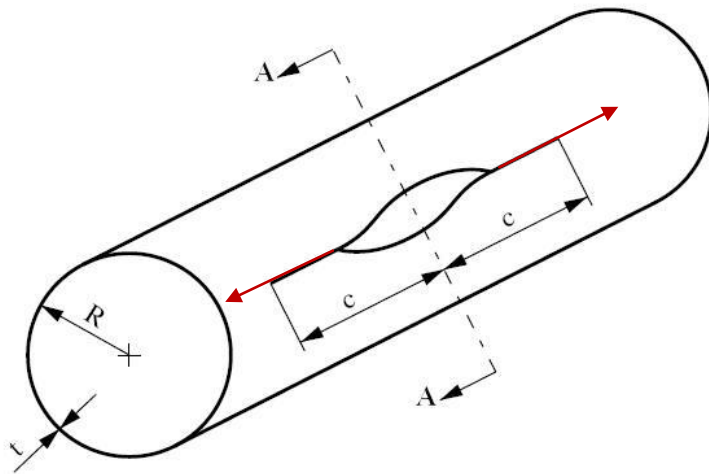


Effects from impurity on pipe design



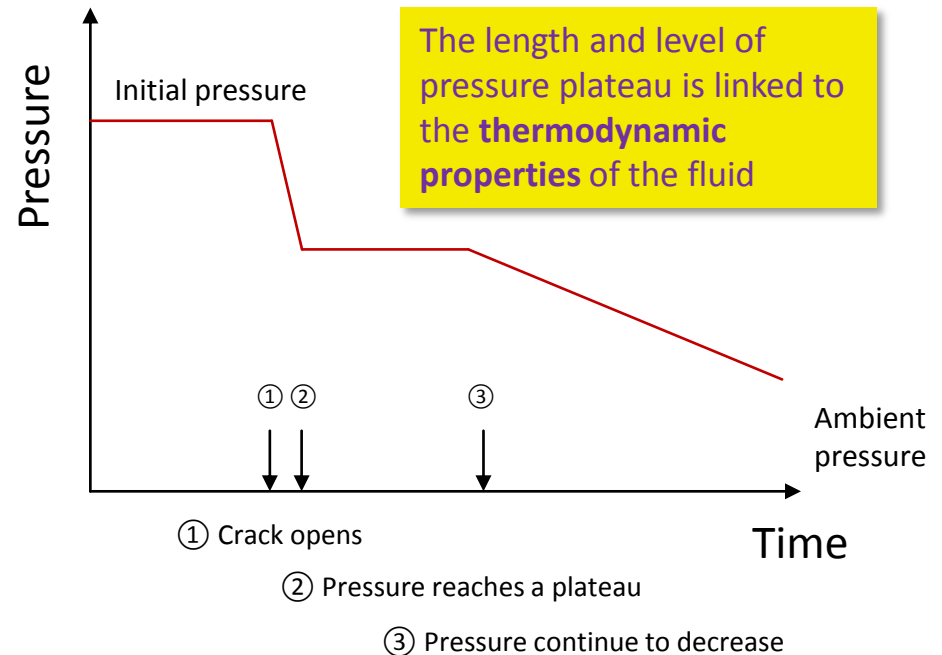
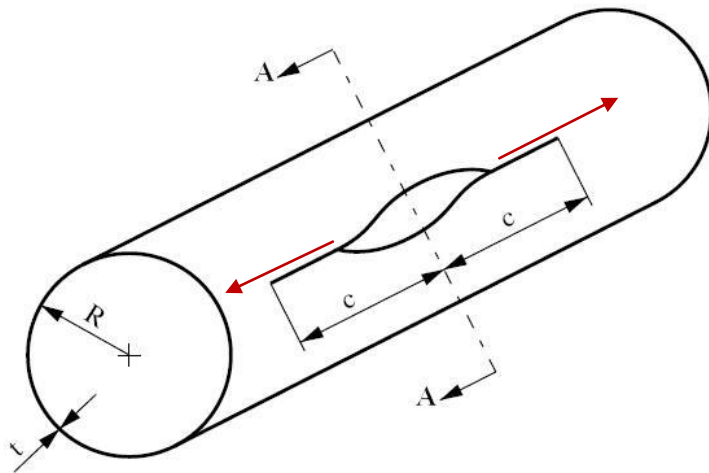
Question: "Will a crack in the pipeline, when initiated, propagate or will it stop?
Known as "Running Ductile Fractures" – or RDF and "crack arrest"

Fracture propagation and pipe design



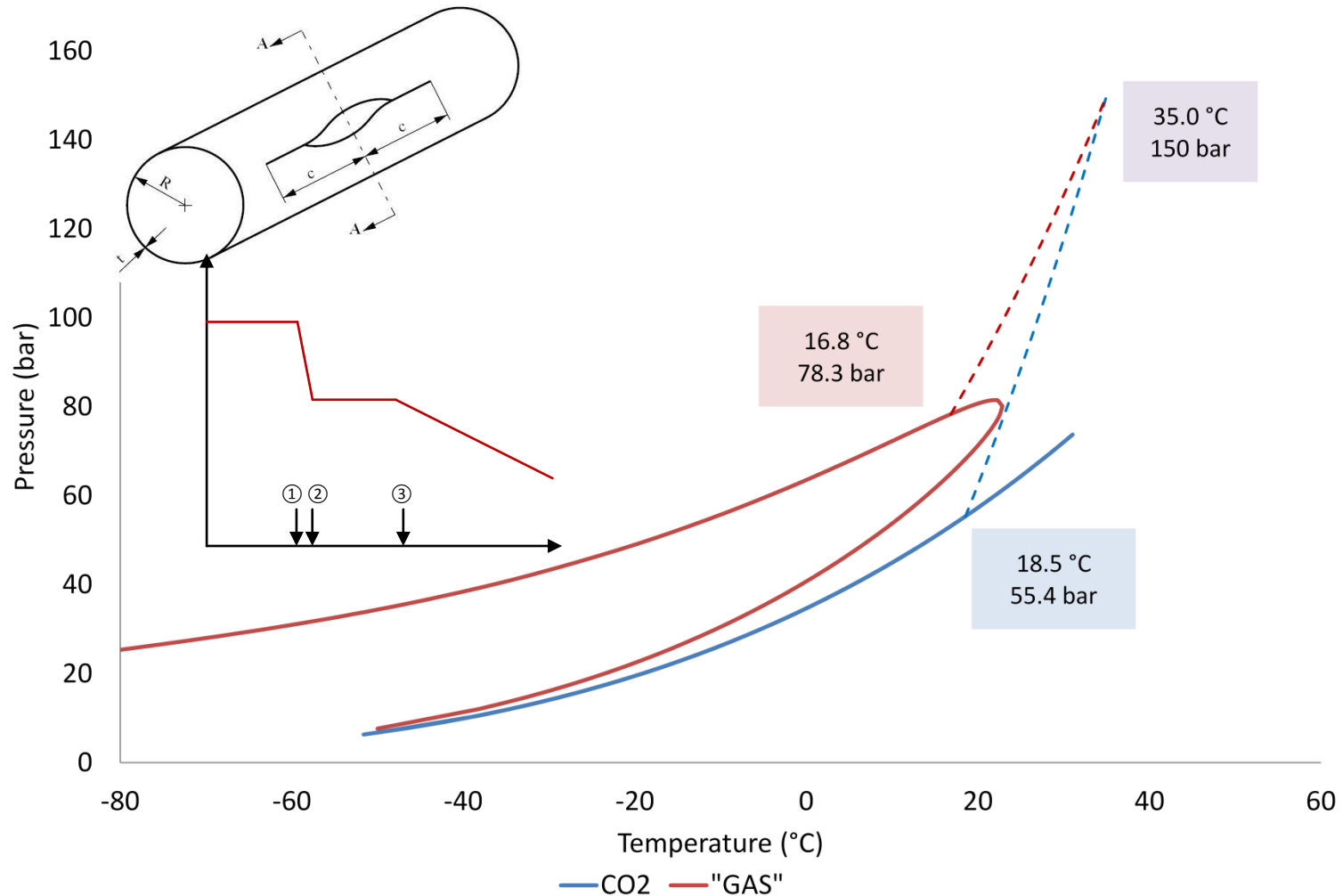
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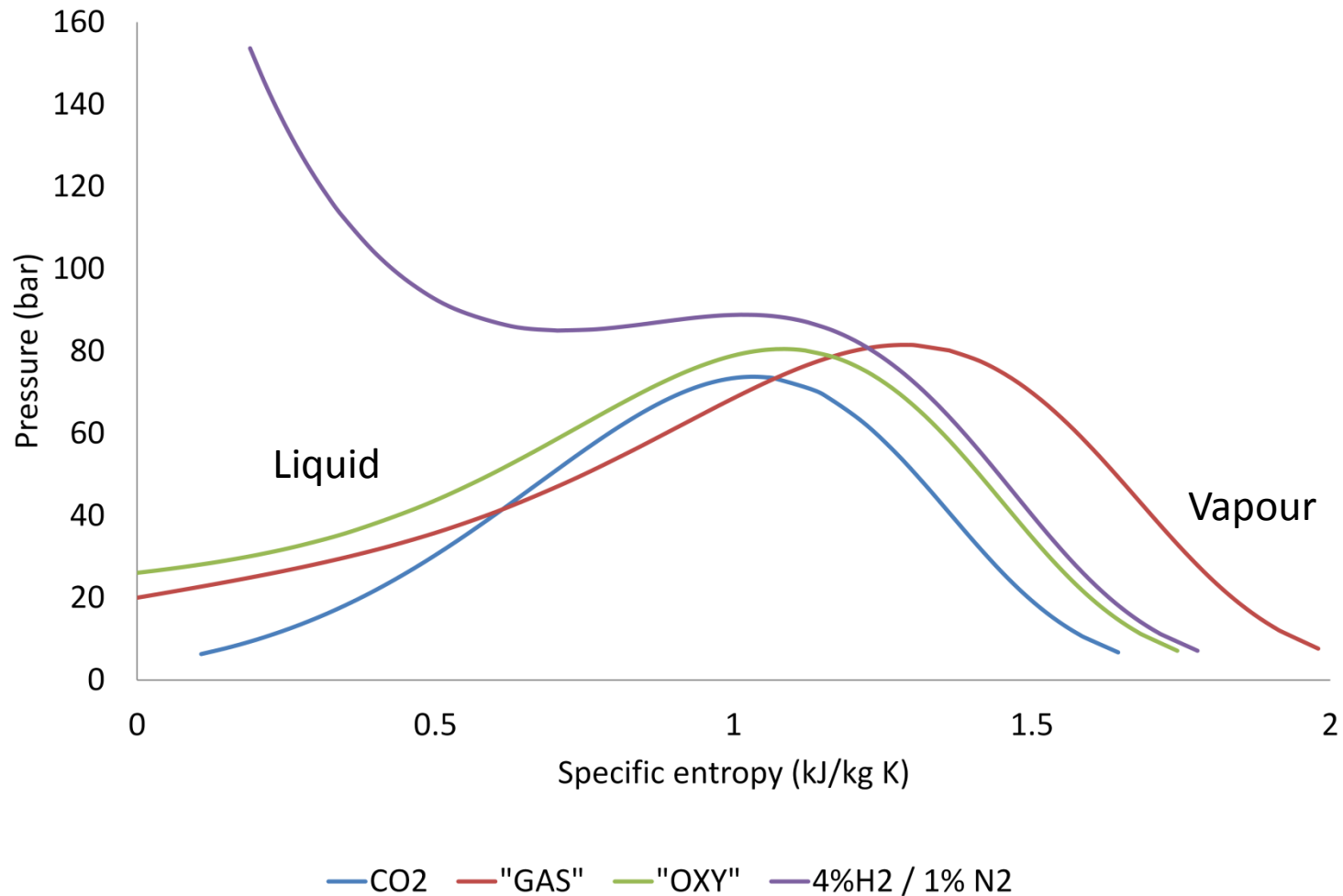


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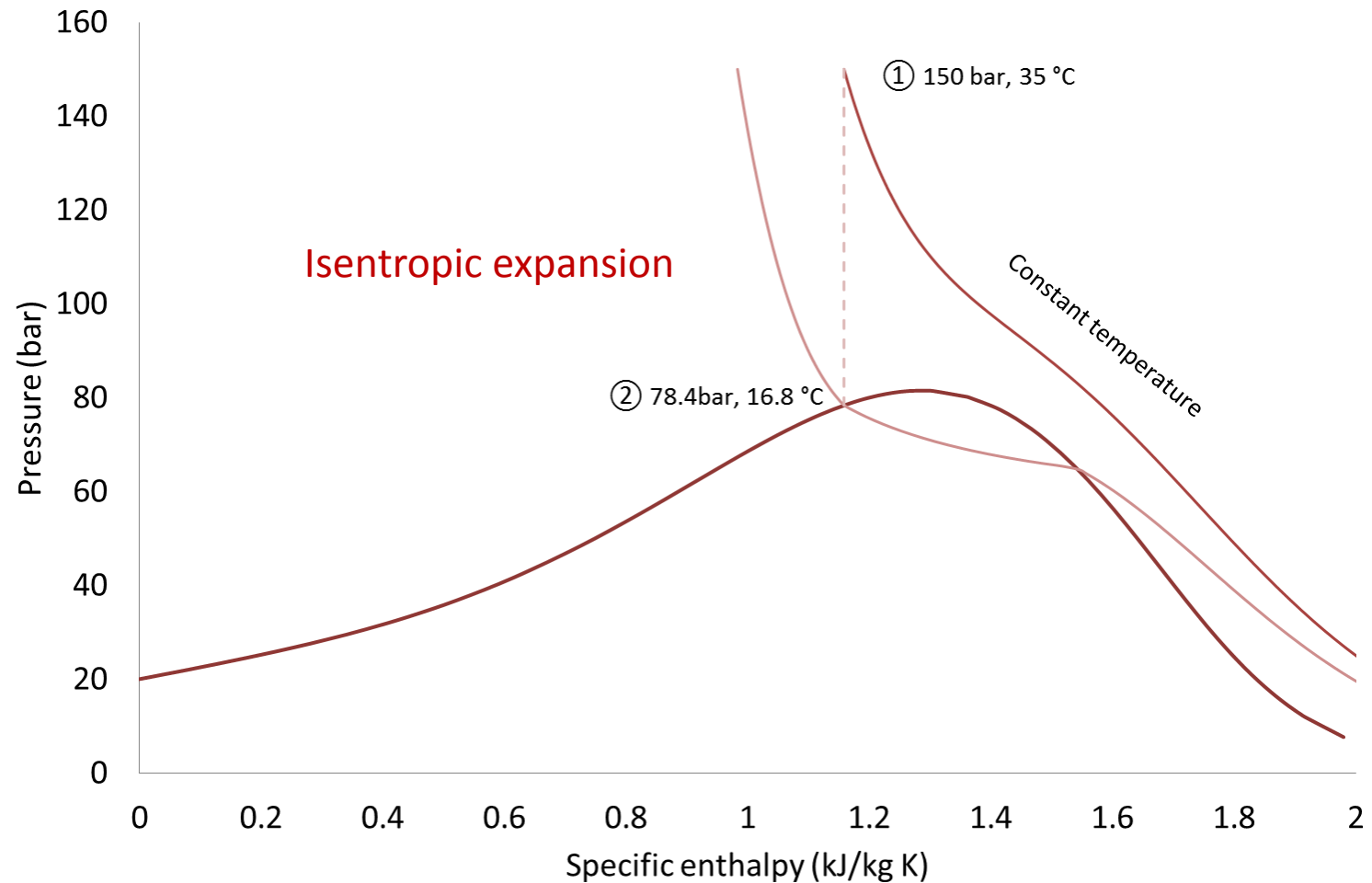
CO₂ phase behaviour – rapid pressure release – isentropic



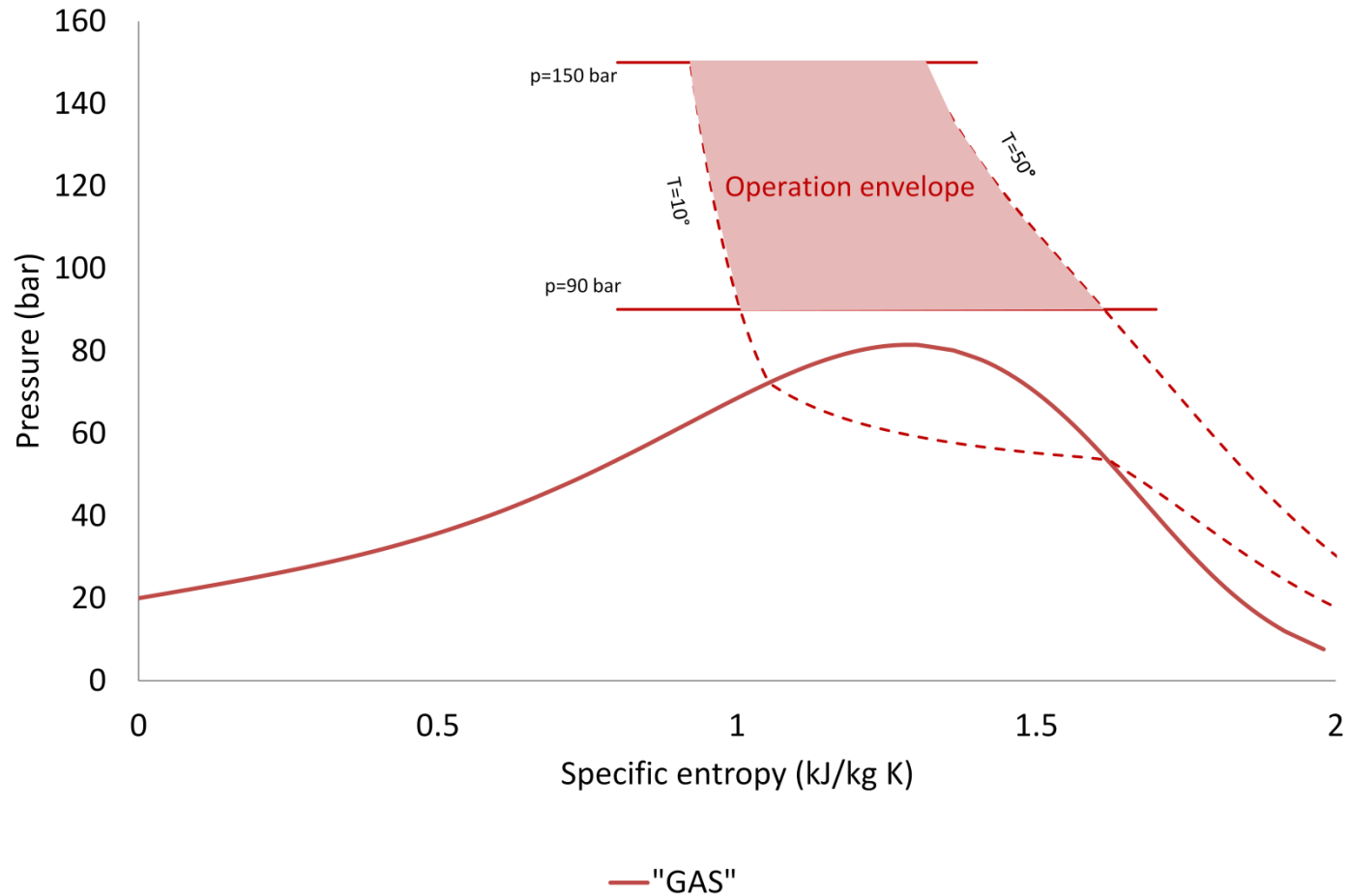
CO₂ phase behaviour with presence of impurities



CO₂ phase behaviour with presence of impurities



CO₂ pipeline operational envelope (Pressure – Entropy)



SMYS and RDF – how does impurities come into the eq.

SMYS – «Specified Maximum Yield Strength»

Wall thickness, t , determined from design pressure, P_D , yield strength, σ_0 and safety factor, f

$$t = \frac{P_D \cdot R_0}{\sigma_0} \cdot \frac{1}{f}$$

RDF – «Running Ductile Pressure»

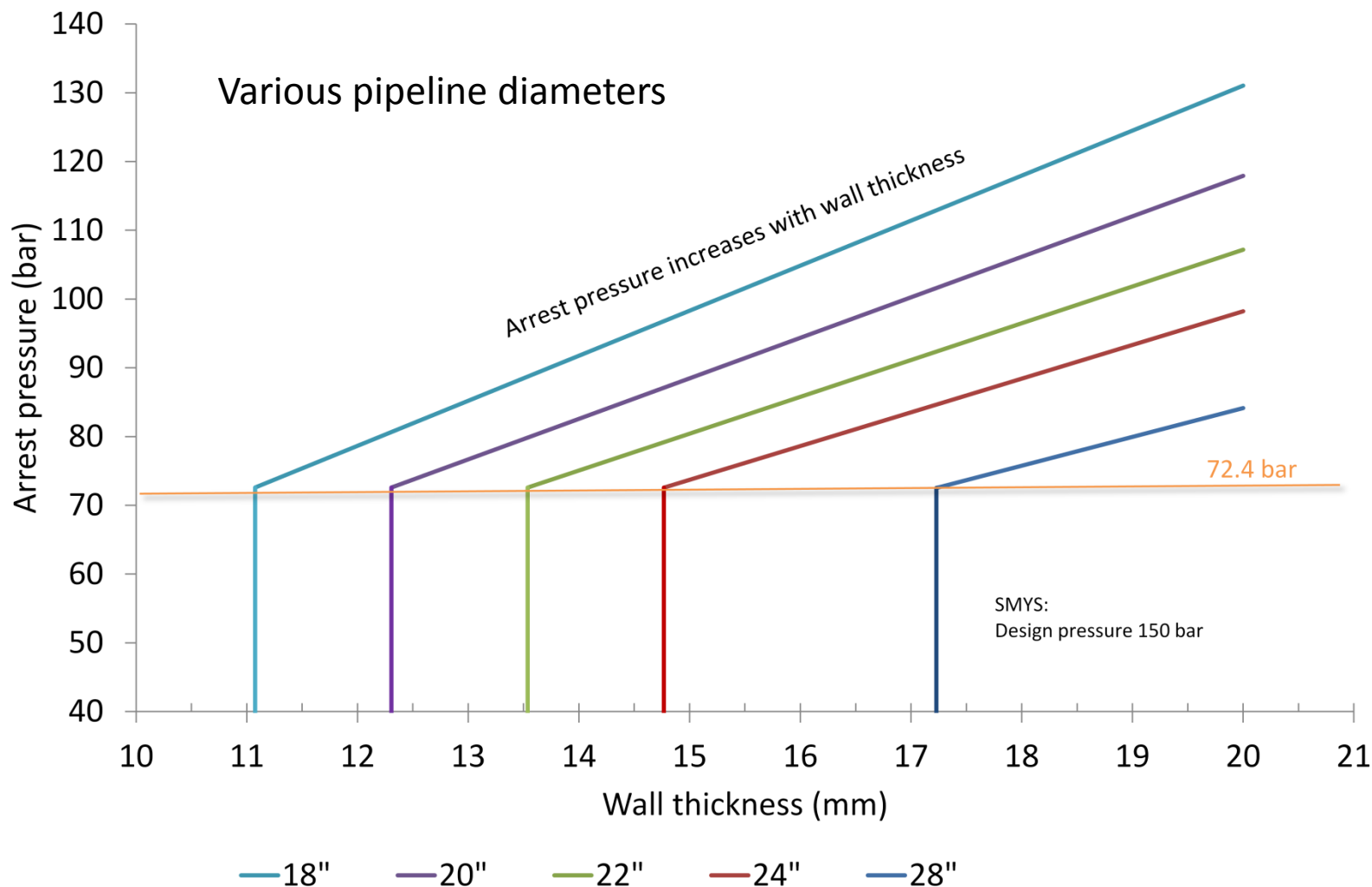
Link between the «saturation pressure» and «arrest pressure»

Very simplified: $p_{\text{sat}} < p_{\text{arrest}}$ then RDF will not occur and a crack will not propagate

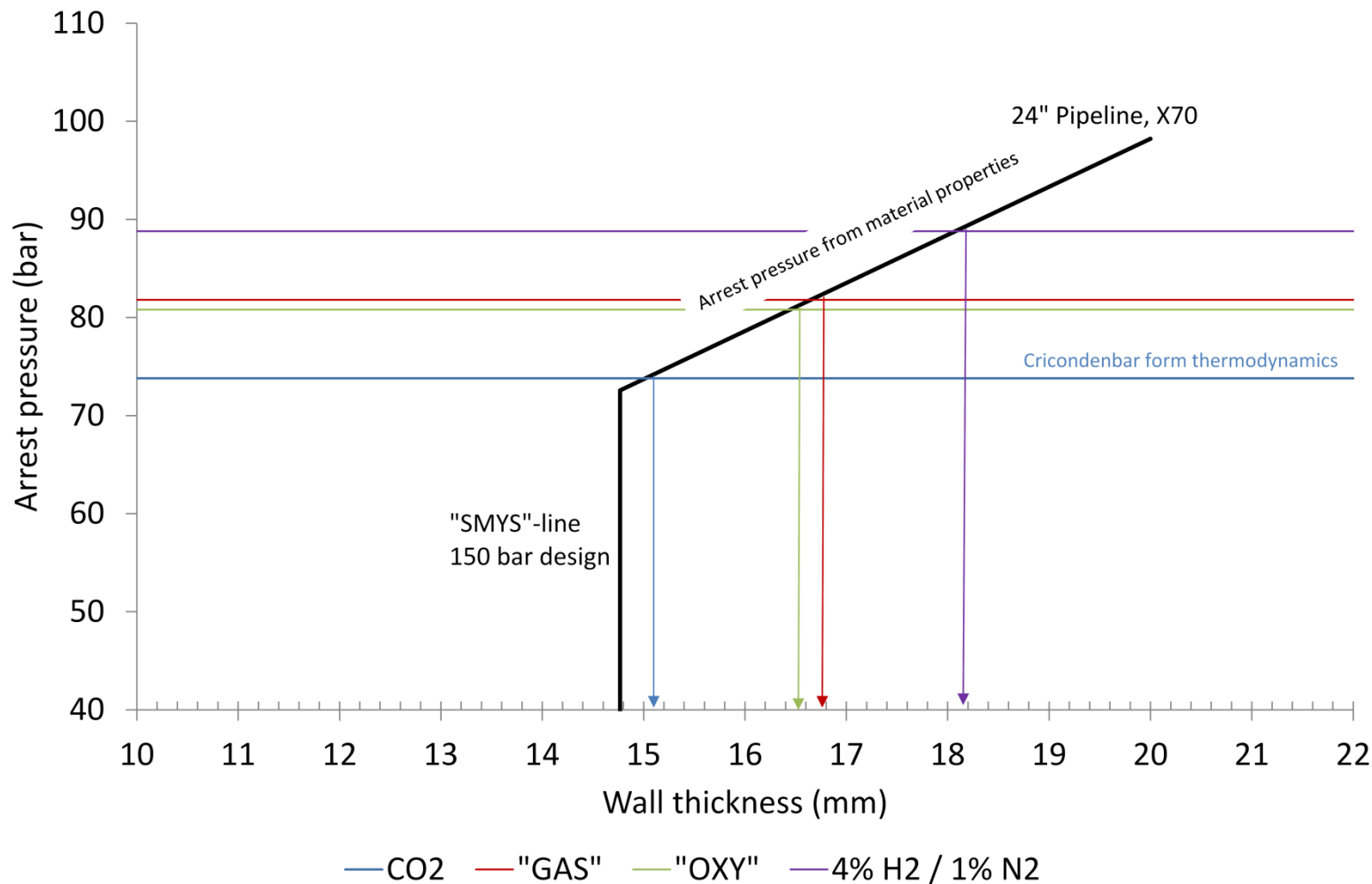
$$p_a = \frac{2 \cdot t \cdot \tilde{\sigma}}{3.33\pi R_0} \cdot \cos^{-1} \left[e^{\left(\frac{\pi R_f E}{24 \tilde{\sigma}^2 \sqrt{R_0 \cdot t}} \right)} \right]$$

From the "Batalle Two-Curve Model"

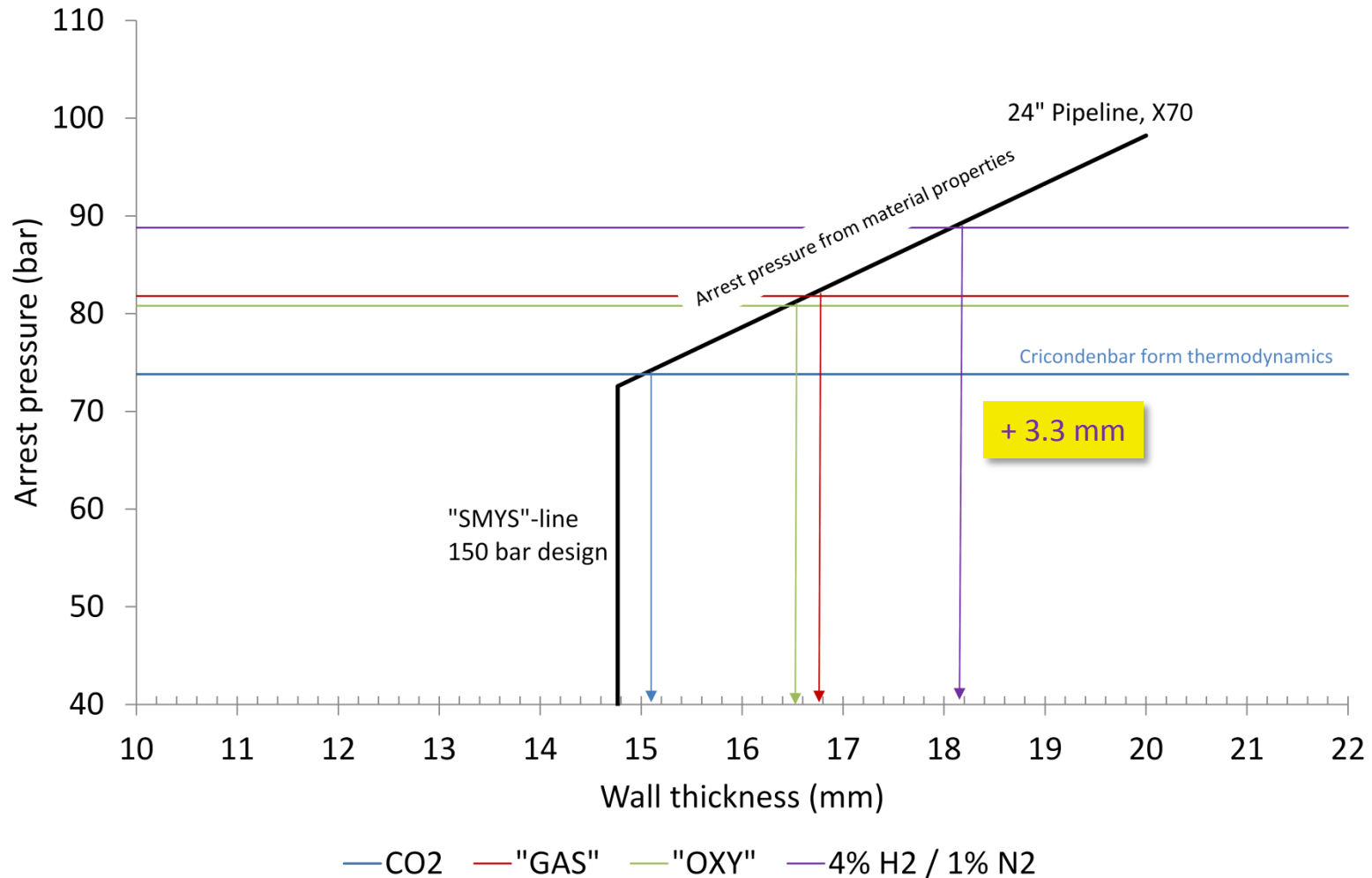
SMYS and RDF – Effect of impurities on wall thickness



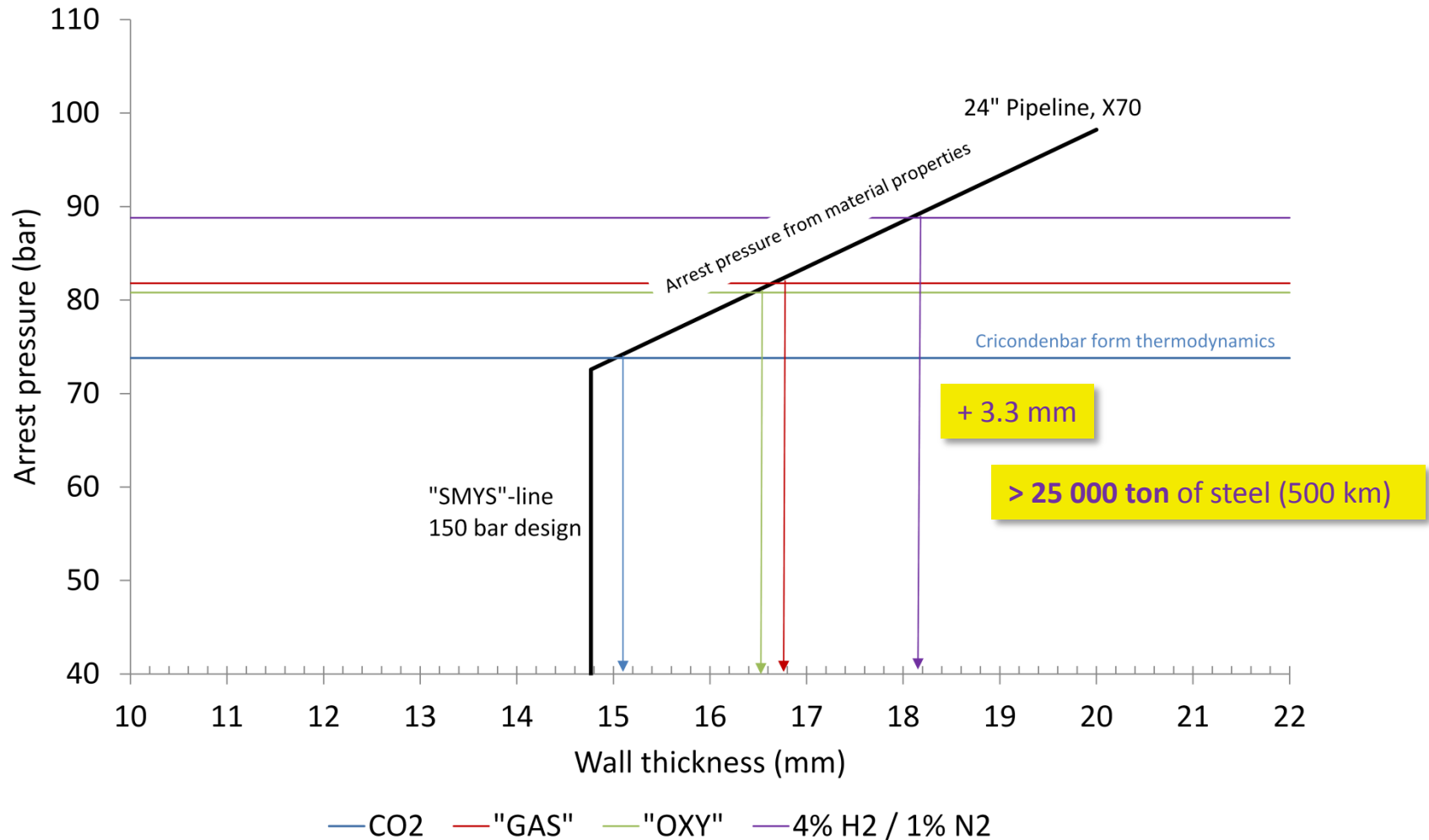
SMYS and RDF – Effect of impurities in a 24" pipeline



SMYS and RDF – how does impurities come into the eq.



SMYS and RDF – how does impurities come into the eq.



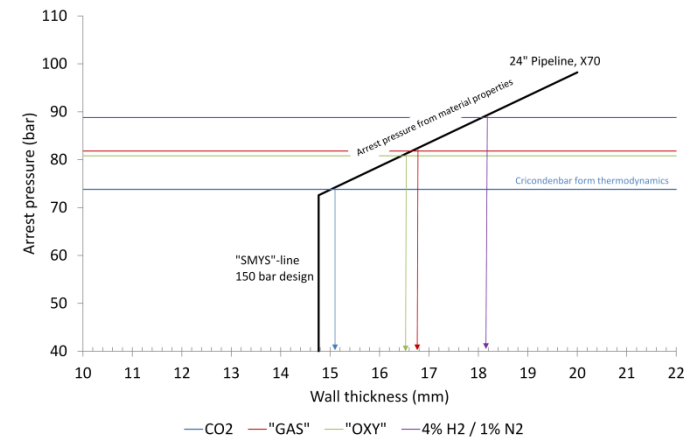
Pipeline sizes used in the analysis

Based on DNV-GL recommendations –
CLASS 3 pipeline: $(SMYS_{0.45} + 1.0 \text{ mm}) + 12.5\%$

Size	Outside diameter	Wall thickness	Inside diameter
	(mm)	(mm)	(mm)
28"	711.2	30.2	681.0
24"	609.6	28.6	581.0
20"	508.0	23.8	484.2
18"	457.2	22.2	435.0

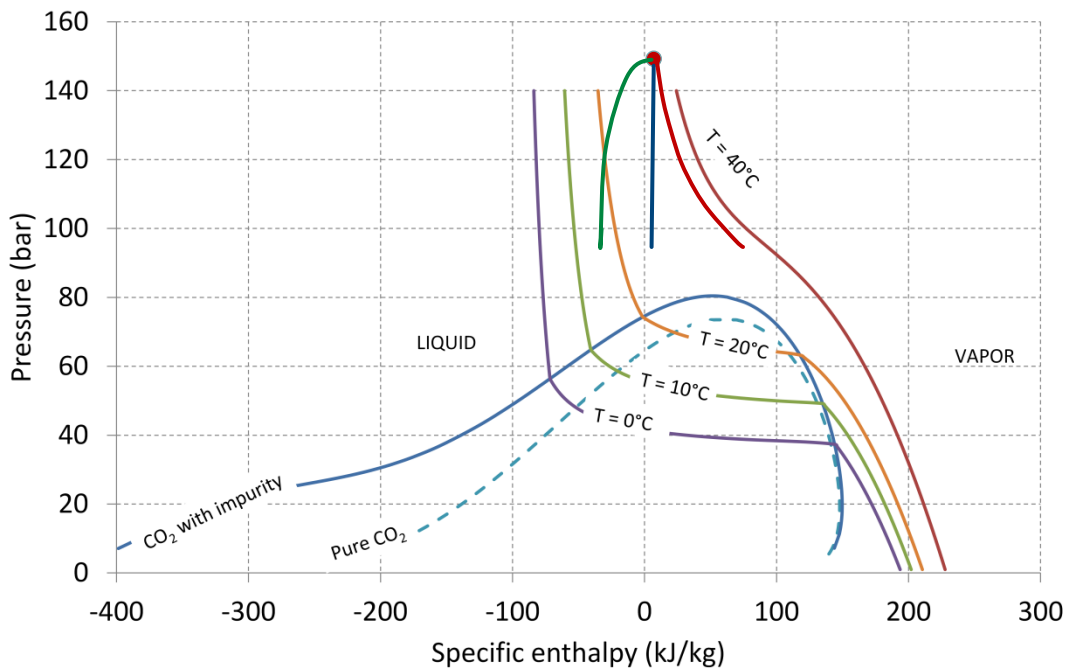
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Possible path for pipeline pressure loss – principle

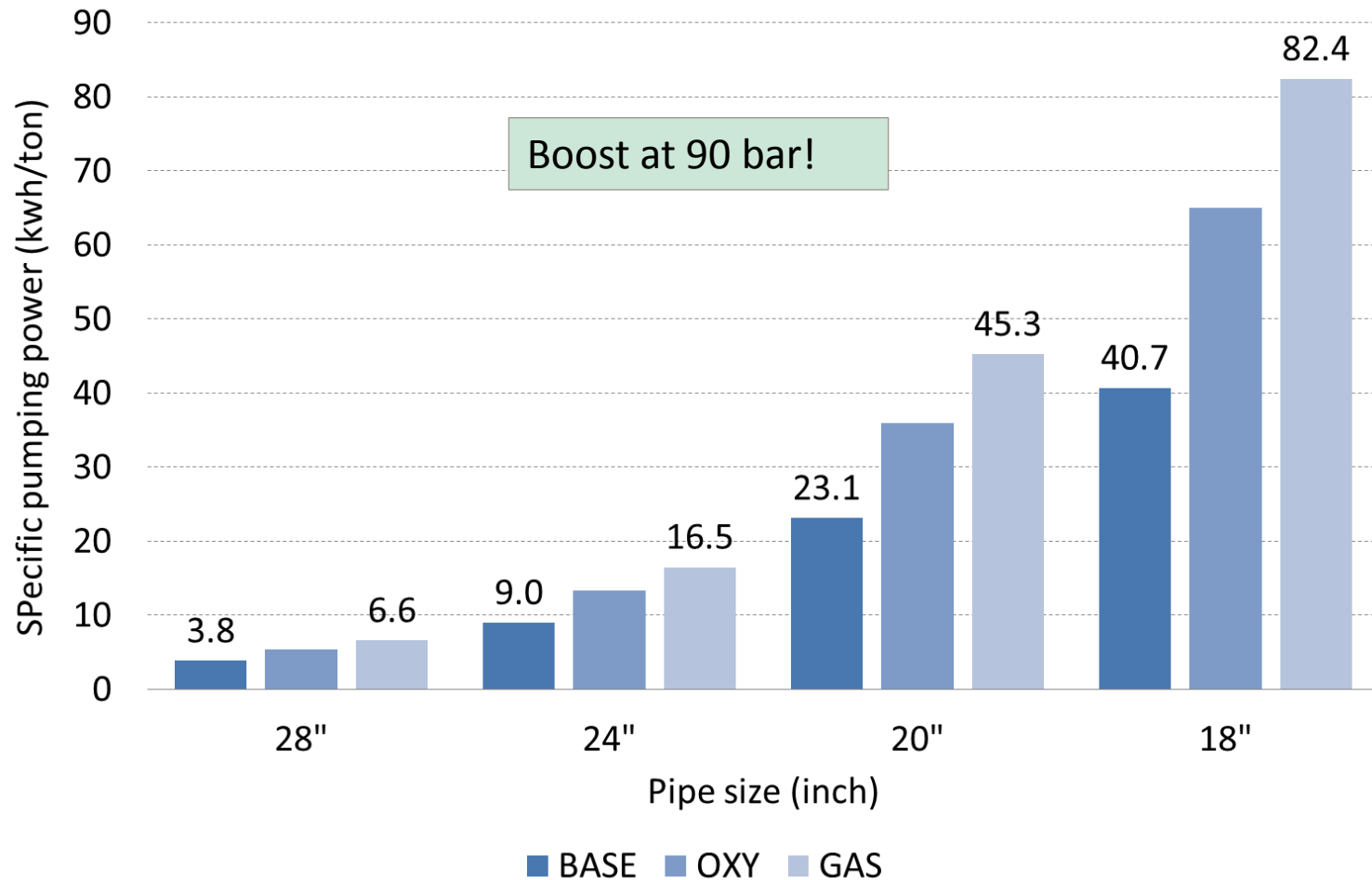


$\text{CO}_2/\text{N}_2/\text{O}_2$ - 4% impurity

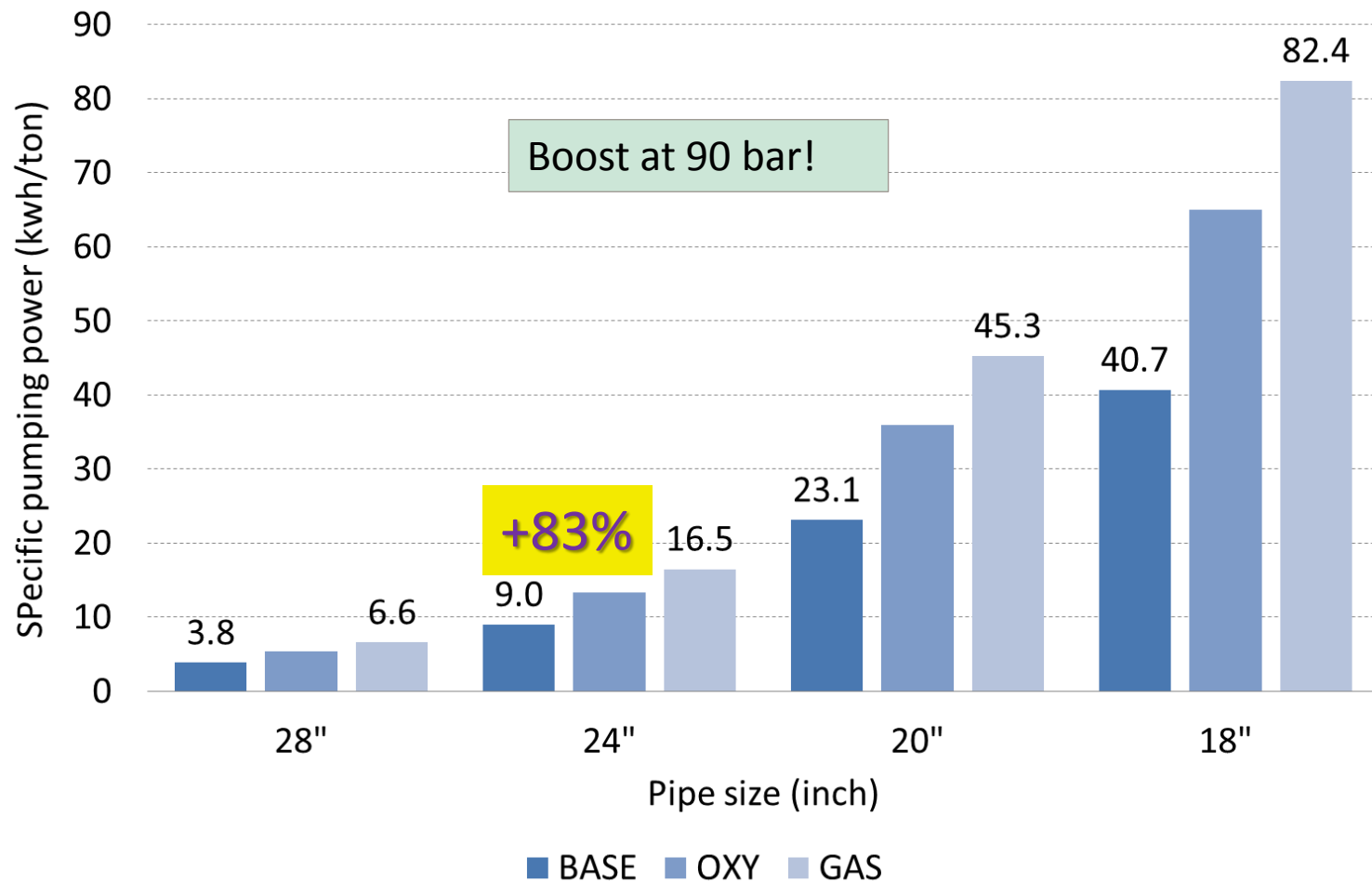
Pressure loss from 150 to 90 bar

- Isothermal
- Adiabatic
- With ambient heat exchange

Power consumption 500 km for on-shore pipeline transport

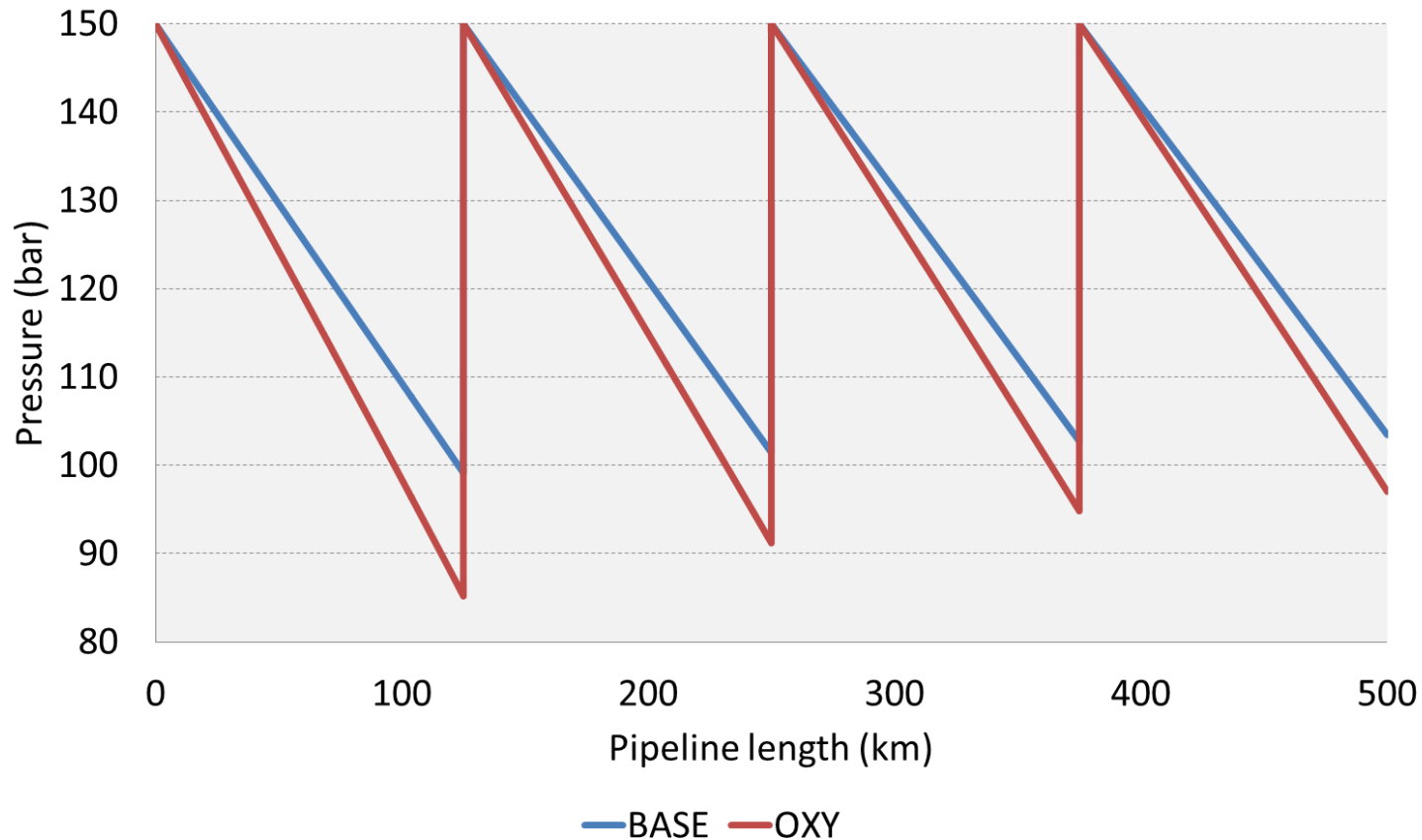


Power consumption 500 km for on-shore pipeline transport



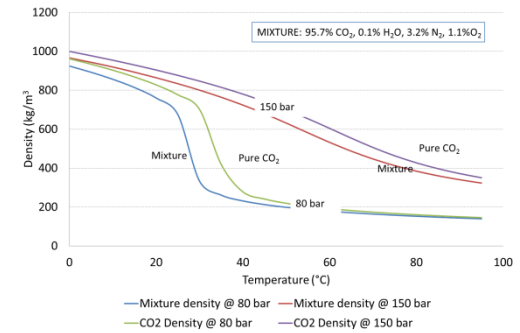
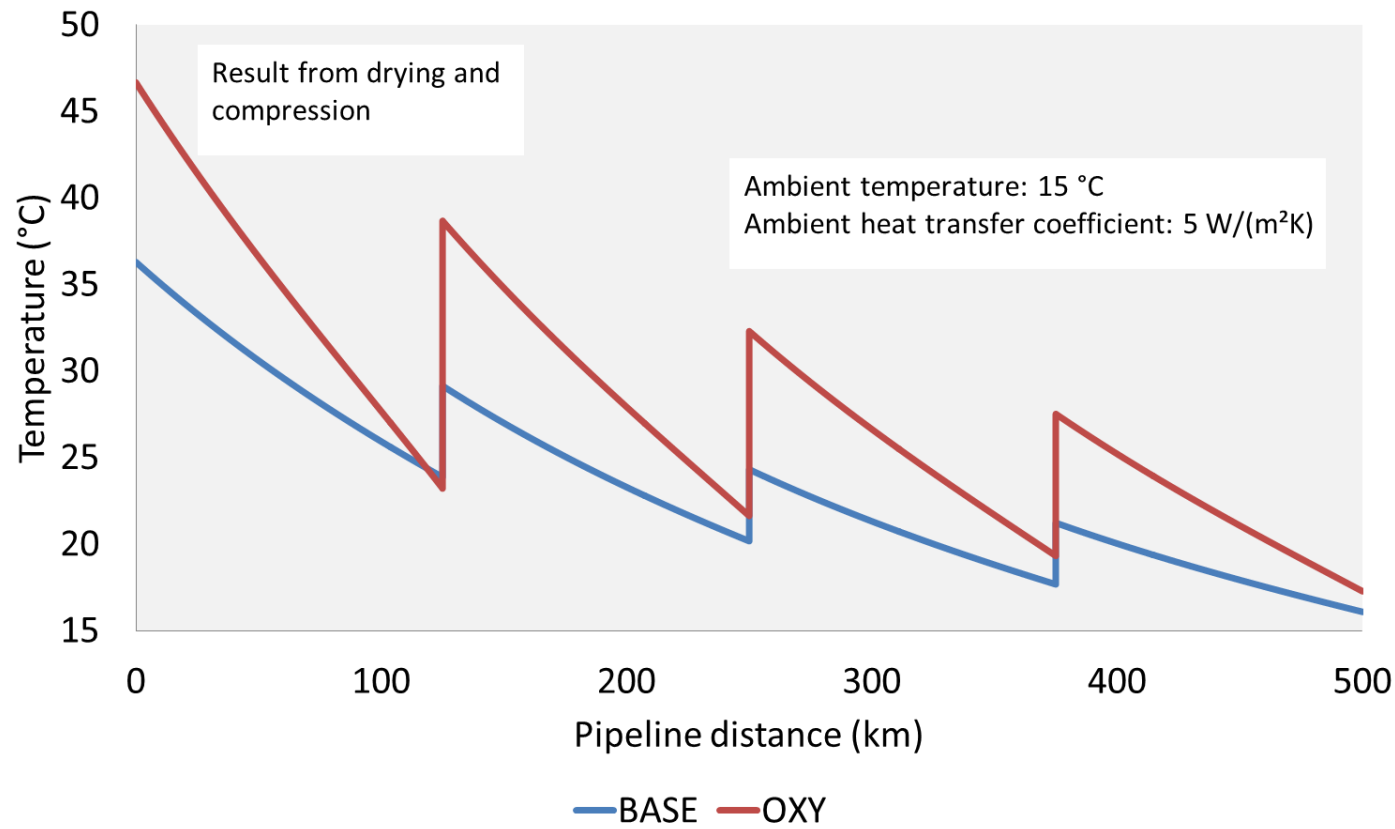
Pressure profile for pipeline transport

24" Pipeline with 4 compressor stations



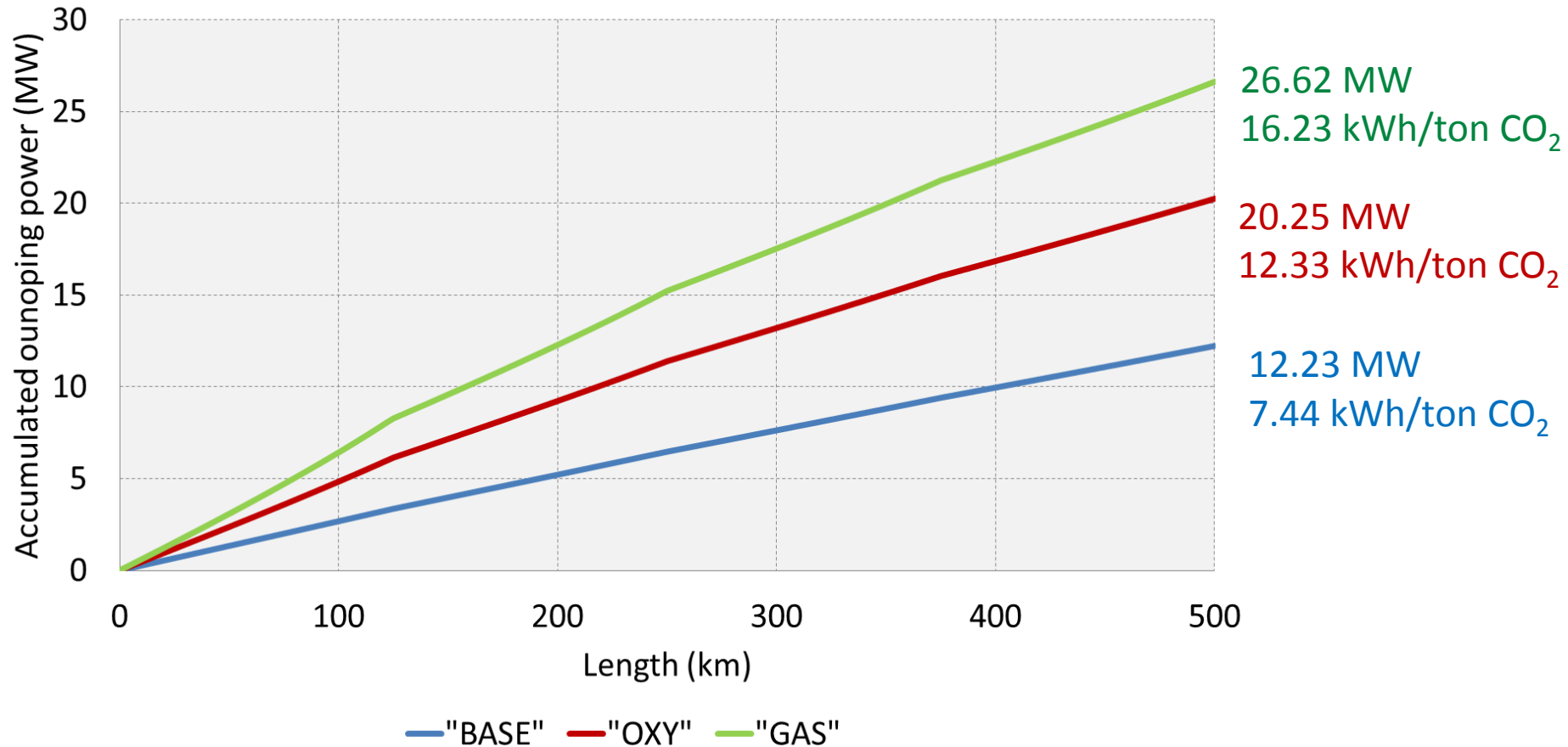
Temperature profile along a 24" pipeline

Temperature profile

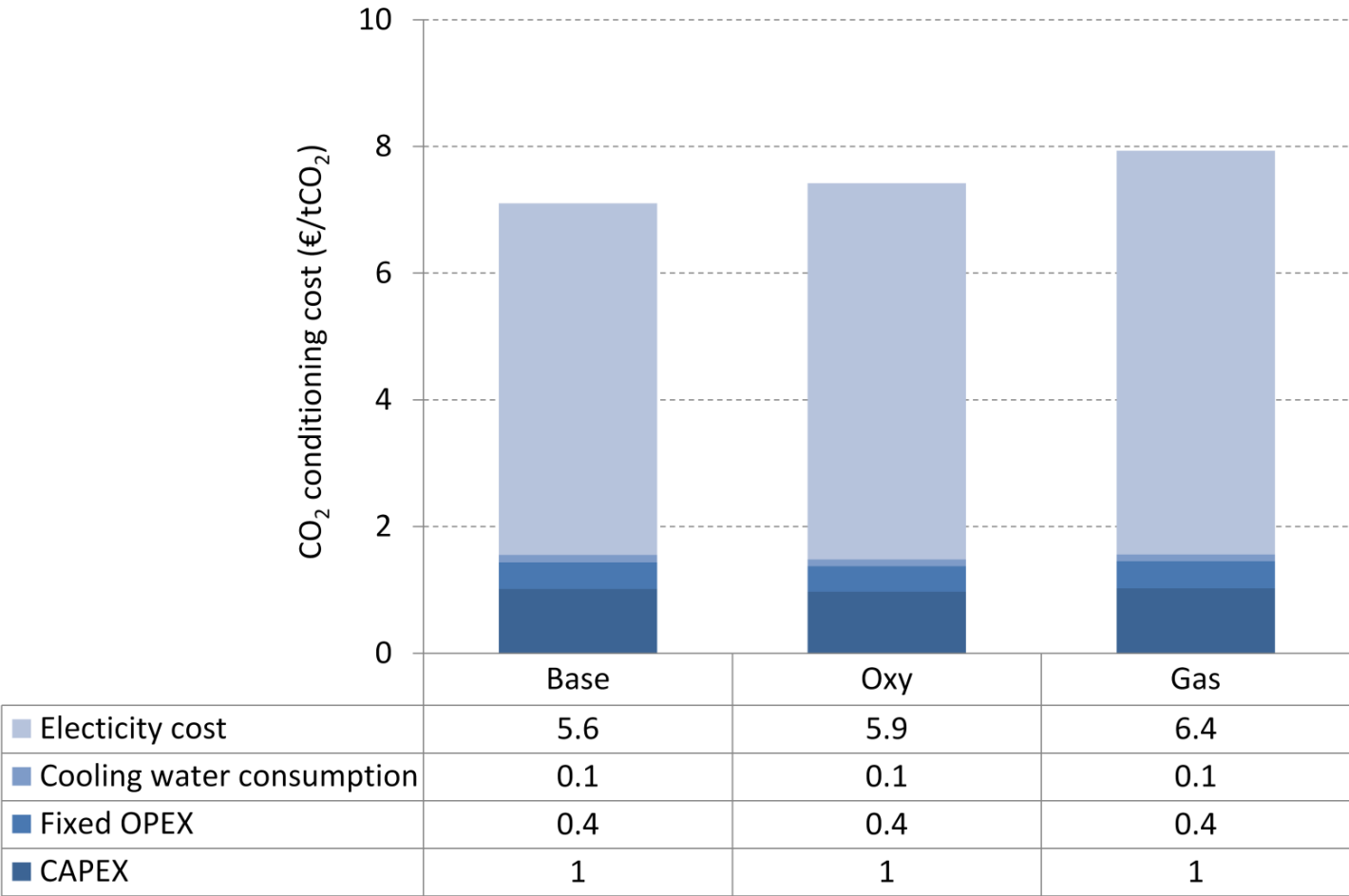


Required pumping power for pipeline transport

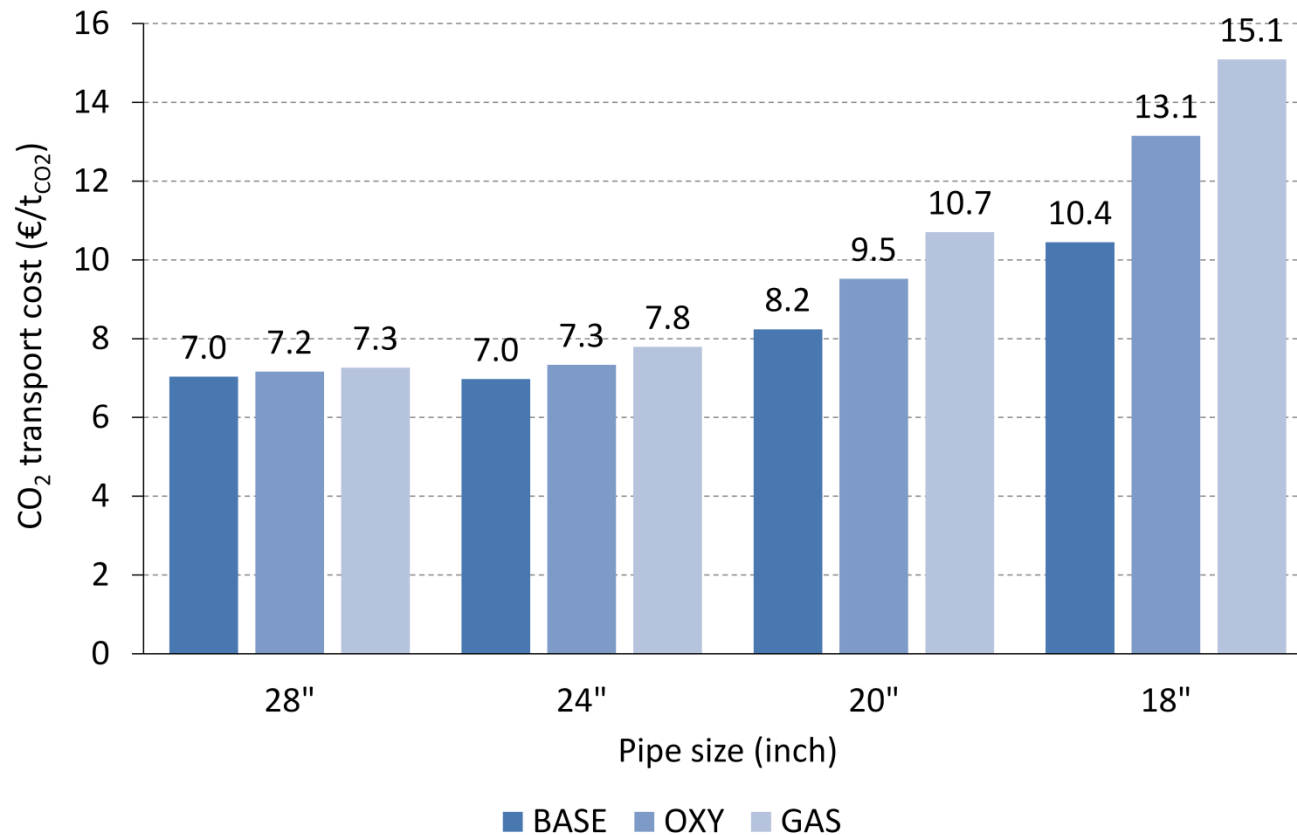
24" Pipeline with 4 booster stations - "pumping power"



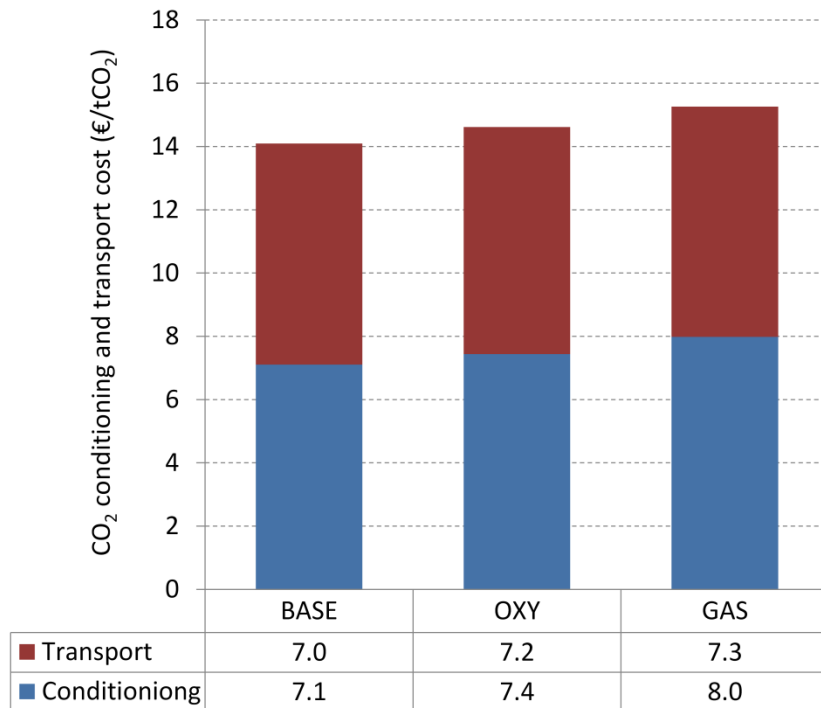
CO₂ conditioning cost of the BASE, OXY and GAS cases, €/tCO₂



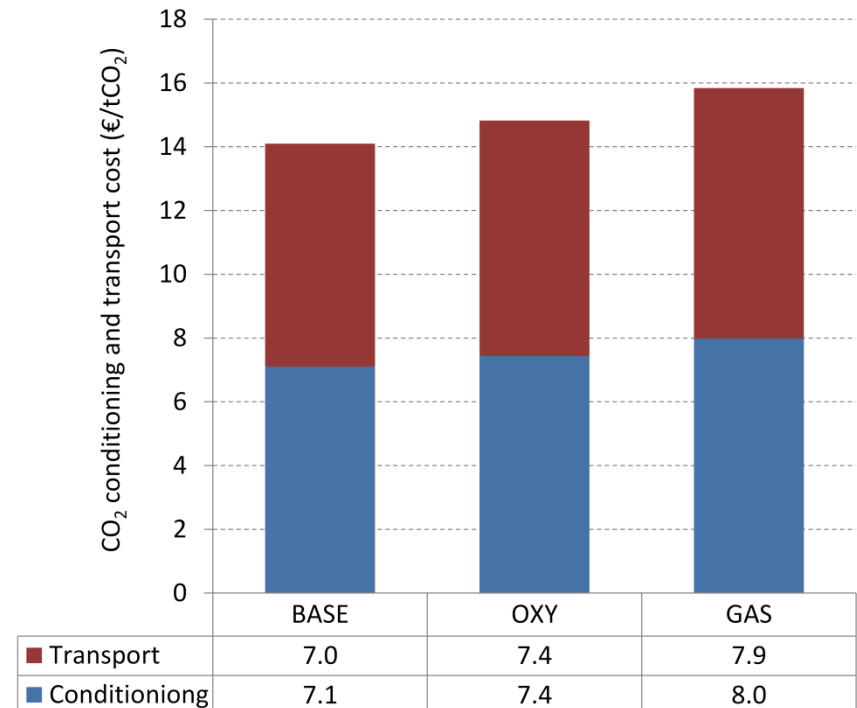
CO₂ transport cost of the BASE, OXY and GAS cases, €/tCO₂



CO₂ conditioning and transport cost



Optimum pipeline diameter



24" pipeline diameter

Summary and conclusions

- Pipeline transport of CO₂ over 500 km
 - The results show that with 4% impurities from N₂ and O₂, the transport power consumption in a 24'' pipeline configuration can increase by 100%
 - to boundary conditions and need to be optimized on a case to case basis
 - The most important thermodynamic property is the density.
- Pipe design
 - It was shown how the cricondenbar for the transported fluid, combined with the possible operational envelope for the transport and the material properties for the pipeline should be used when evaluating the potential for RDF
- Economics:
 - The results showed a cost increase of 8.5% annually for conditioning and transporting CO₂ with impurities in a pipeline optimized for pure CO₂

Thank you for your attention!

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